# Rutile Concentration by Reduction of Titanium Ore -Laterite Mixture Using Biomass

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**Abstract** Rutile is a mineral which is used in making paints, ointments, tooth paste, sunscreens, just to mention a few products. Titanium metal makes alloys with less density and resistance to corrosion, which are used in making aircraft and marine vessels. Rutile is obtained from ores by concentration method using chemicals, a process which is very expensive. In this paper, we have investigated on alternative method of concentrating rutile from titanium ores. This was done by reduction of the mixture of titanium ore and laterite using biomass. The titanium ores were obtained from Maragwa location in Tharaka Nithi County and mineralogical and chemical composition carried using XRD and AAS. The mixture of 25 g of the ore, 2 g of laterite and 1.0 g of ground dry biomass was put into clay pots. The samples were placed in a charcoal burner and heated at temperature range 800 - 900°C for two hours and the temperature monitored using a thermocouple. After two hours the sample mixtures were cooled to room temperature and serial magnetic separation done. The samples were digested and analyzed for rutile using AAS and XRD. The results show that rutile composition increased from about 0.40% in raw ore to about 2.62%, which represents 2.22% increase. This percentage increase varies depending on the ore mineralogy and chemical composition. Therefore, titanium ores with low concentration of iron can be concentrated using laterite rich in iron. Besides obtaining rutile, the method offers a successful way of cleaning the environment by using biomass from municipal waste.

Keywords Laterite, Biomass, Reduction, Rutile, Concentration

## **1. Introduction**

The concentration of titanium in low grade titanium ores in laterite has been done by heating the raw laterite sample with lantana camara and separated using a strong magnet [7]. In their work, the concentrate obtained after reduction at temperature rage 500 to 800 °C was manly maghemite and titanomagnetite. Another study done on the effects of temperature on the ilmenite containing laterite, confirmed that concentration of titanium was possible using biomass at the temperature range of 800 - 1200° [3]. A South African company known as Richards Bay Minerals (RBM), extract rutile from ilmenite containing ores by reduction using carbon at temperature range of 730°C to 800°C [8].

The recovery of rutile from synthetic industrial waste has been investigated using caustic hydrothermal method [1]. The method involved decomposition of the industrial ilmenite waste and then followed by the sulphate process to obtain rutile. Studies on extraction of rutile from beach sand has been done [4]. In their investigation, Perez & Sharadqah

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Received: Dec. 28, 2021; Accepted: Jan. 26, 2022; Published: Feb. 24, 2022 Published online at http://journal.sapub.org/materials [4] first heated the samples to remove impurities which were difficult to be removed by conventional physical or mechanical treatments. The second step involved mixing the samples with sodium hydroxide pellets and later heating at 1100 °C. The products obtained were then hydrolyzed to obtain hydrated titanium dioxide. The hydrated product was then digested using acid in the presence of iron metal as reducing agent to obtain about 92 percent TiO<sub>2</sub>.

Another method of obtaining very high-grade synthetic rutile has been developed [6]. In their study, Ilmenite was roasted at temperature ranges of 800 °C to 1,000 °C to selectively magnetize the ilmenite fraction. The ilmenite was able to be removed through magnetic separation leaving out the gangue. Iron and other impurities were removed by leaching process at normal conditions and hydrochloric acid. The leached solid content was washed, filtered, and calcined to produce a synthetic rutile grading at about 97 percent.

## 2. Methodology

#### 2.1. Sample Collection and Preparation

Samples for analysis were obtained from Maragwa location, Tharaka North Sub - County in Tharaka Nithi County at locations 0°18'S38°8'E and 0°21'S38°11'E.

Random sampling was done from five quarries which were within one to two kilometers apart from each other. Three sampling sites from each quarry were selected within a distance of about 10m apart. A mattock and a shovel were used to break the rocks and scoop out the mineral respectively. Mineral samples were obtained from a depth of 30cm from each of the 3 sites and crushed into small particles using a hammer. The crushed mineral particles were mixed carefully and then about two kilogram of it was obtained and packed in labeled plastic bags for analysis.

#### 2.2. Sample Preparation for XRD and Analyses

About 30g of pulverized mineral samples to 250 micro millimeters using a ball mill was put into the sample holders. The samples were then loaded in X - ray diffractometer for analysis of minerals using data collector software [5], [2].

### 2.3. Sample Preparation for AAS and Analyses

About 0.1 g of the sample was weighed and put in a 125-ml plastic container. One ml of concentrated aqua-regia (1:3, Nitric acid to hydrochloric solution) was added followed by 3.0 ml of hydrofluoric acid. The sample was then left to digest for at least 8 hours. 50.0 ml of saturated boric acid was added then allowed to react for one hour. The solution content was then topped up to make 100.0 ml using distilled water. Samples were then analyzed alongside the standards [2].

## 2.4. Concentration of Titanium from Ore - Laterite **Mixture Using Biomass**

#### 2.4.1. Optimisation Studies

A mixture of 5.0 g of the ore, 2.0 g of ground laterite and

1.0 g of ground biomass was put into clay crucibles. The clay crucibles were placed into the charcoal burner and heated at a temperature range of 800 - 900°C for two hours. The temperature was monitored using a thermocouple. After two hours the sample mixtures were cooled to room temperature and serial magnetic separation done as per [5] and [2]. The samples were digested and analyzed for rutile using AAS and XRD.

The experiment was repeated by varying the mass of ore from 5.0 g to 40 g at an interval of 5.0 g. The masses of the biomass mixture were held constant at 1.0 g and that of laterite at 2.0 g. The reduction temperature was maintained at 800 - 900°C. The separation was done as explained above and samples digested and analyzed for rutile using AAS and XRD.

## 3. Results and Discussion

#### 3.1. Mineralogical and Chemical Composition of Laterite

The laterite from Gitong'o in Tharaka Nithi County was used to enrich the ilmenite ore during reduction. The results of its mineralogical and chemical composition are given in fig. 1 and table 1.

The results of, rutile composition was low while that of silica was high followed by iron oxides. The sample also contained alumina which was likely to influence the rutile composition in the laterite. The laterite was used to investigate on the chemical transformation during concentration of titanium in the ores in the presence of biomass. The XRD results of the sample 3231, before reduction and that of the tailing and the concentrate is given in fig. 2, 3 and 4 respectively.

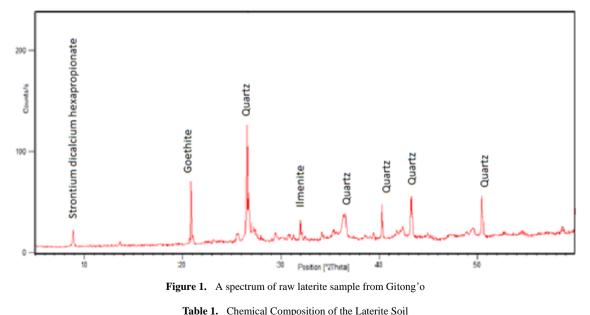


Table 1.	Chemical	Composition	of the	Laterite Soil
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Sample	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	K <sub>2</sub> O	Na <sub>2</sub> O	CaO	TiO <sub>2</sub>	MnO	Fe <sub>2</sub> O <sub>3</sub>	MgO	LOI
Source	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE
Gitong'o	$45.48 {\pm} 0.12$	$17.15 \pm 0.07$	$0.02 \pm 0.03$	$0.04{\pm}0.02$	$0.04{\pm}0.03$	$0.27{\pm}0.01$	$0.21 {\pm} 0.03$	29.31±0.01	$0.24{\pm}0.02$	$5.12 \pm 0.03$

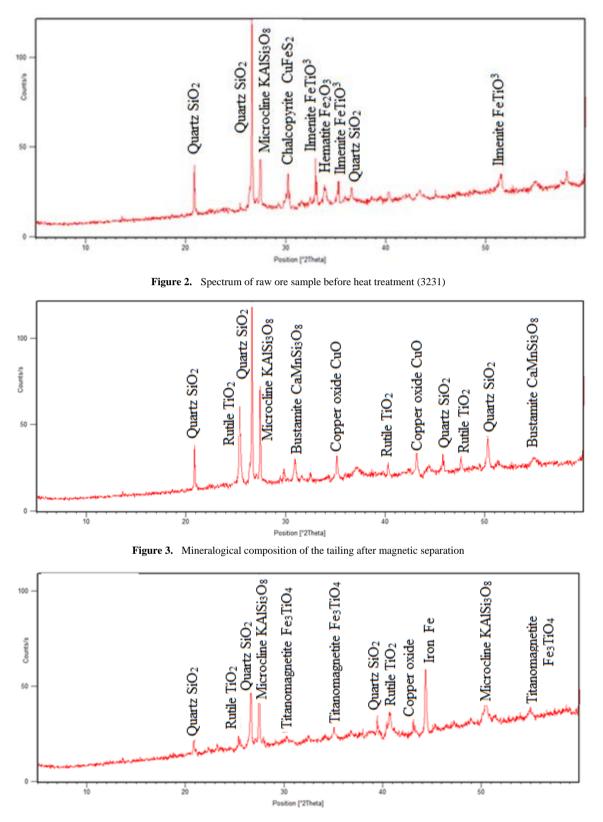


Figure 4. Mineralogical composition of the magnetic sample after magnetic separation

The results from figure 3 show that, after heat treatment ilmenite and hematite peaks disappeared and rutile peak appeared at two angle theta  $25^{\circ}$ ,  $40.5^{\circ}$  and  $48^{\circ}$  in fig. 4. In the same fig. 4, Titanomagnetite peak appeared at angle theta  $30^{\circ}$ ,  $35^{\circ}$  and  $55^{\circ}$  and the iron peak was found at two angle

theta 44.5°. This means that iron minerals were able to be reduced to iron at temperature range of 800 - 900°C. The intensity of rutile peak in non-magnetic sample shows that much of rutile was collected in the tailing. The chalcopyrite mineral peak disappeared and copper oxide peaks are both found in fig. 3 and 4 at two angle theta  $35^{\circ}$  and  $43.5^{\circ}$ . The formation of CuO was probably due to the re-oxidation of copper during cooling. Chemical analysis was done, and the results given in table 2.

The results show that rutile composition ranged from 0.41 to 1.13 percent. These values though very low, were used to investigate the concentration of ore-laterite mixture using biomass. The optimized results of sample 3231 are given in the table 3.

The results show an increase from 0.46 percent obtained in raw sample to 1.48 percent after reduction using ore, laterite and biomass mixture. The results from table 3 show that the mixture of 25 g of the ore, 2 g of the laterite and one gram of biomass gave good results of the concentrated rutile. From literature, goethite and hematite minerals are converted to magnetite minerals at temperature range of 500 - 700 °C [7], [5], [2]. This is shown in equation 1 and 2.

$$\operatorname{Fe}_{2}O_{3} \cdot \operatorname{H}_{2}O_{(s)} \xrightarrow{500-700^{\circ}\mathrm{C}} \operatorname{Fe}_{2}O_{3(s)} + \operatorname{H}_{2}O_{(g)} \quad (1)$$

$$3Fe_2O_{3(s)} + CO_{(g)} \xrightarrow{500-700^{\circ}C} 2Fe_3O_{4(s)} + CO_{2(g)}$$
 (2)

According to [7], ilmenite minerals are also oxidized by syngas to form magnetic susceptible titanomagnetite minerals at the same temperature range. This is shown in equations 3, and 4.

Table 2. Elemental Analysis of Raw Samples Using AAS

Oxides	SiO <sub>2</sub>	$Al_2O_3$	K <sub>2</sub> O	Na <sub>2</sub> O	CaO	TiO <sub>2</sub>	MnO	Fe <sub>2</sub> O <sub>3</sub>	Cu	CuO	MgO
Sample Reference	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean±SE	Mean ±SE	Mean ±SE	Mean ±SE	Mean ±SE
3230	41.51± 0.08	8.13± 0.05	7.76± 0.05	12.85± 0.07	2.28± 0.02	0.41± 0.06	0.11± 0.02	3.82± 0.03	9.60± 0.01	12.00± 0.01	5.81± 0.02
	0.08	0.05	0.03	0.07	0.02	0.00	0.02	0.03	0.01	0.01	0.02
3231	44.96±	$5.47\pm$	$4.87\pm$	6.08±	$19.03\pm$	$0.46\pm$	$0.80\pm$	$7.58\pm$	$4.42\pm$	$5.52\pm$	3.73±
5251	0.13	0.01	0.02	0.05	0.07	0.03	0.02	0.04	0.02	0.02	0.02
3232	42.73±	11.47±	10.43±	3.87±	$2.60\pm$	1.13±	0.14±	$17.60\pm$	2.76±	$3.45\pm$	5.55±
3232	0.08	0.05	0.03	0.04	0.01	0.09	0.01	0.03	0.02	0.02	0.04
3233	25.84±	9.17±	6.84±	3.69±	1.31±	0.91±	0.21±	$40.92\pm$	$4.43\pm$	5.54±	3.14±
5255	0.05	0.06	0.01	0.02	0.01	0.03	0.03	0.10	0.02	0.03	0.04
2242	39.73±	7.65±	1.70±	5.24±	12.91±	1.06±	0.28±	20.26±	6.69±	8.35±	3.22±
3242	0.04	0.10	0.01	0.06	0.02	0.06	0.02	0.09	0.01	0.01	0.02

Mass of biomass (g)	Mass of the ore (g)	Mass of laterite (g)	$\%\ TiO_2$ from non-magnetic portion after reduction of ore - laterite mixture using biomass	% TiO <sub>2</sub> from magnetic portion after reduction of ore - laterite mixture using biomass
1.0	5.0	2.0	0.97	0.02
1.0	10.0	2.0	1.18	0.03
1.0	15.0	2.0	1.32	0.02
1.0	20.0	2.0	1.42	0.03
1.0	25.0	2.0	1.48	0.03
1.0	30.0	2.0	1.35	0.01
1.0	35.0	2.0	1.31	0.02
1.0	40.0	2.0	1.01	0.02
1.0	45.0	2.0	0.91	0.03
1.0	50.0	2.0	0.19	0.02

 Table 3.
 Optimized Results After Reduction of Ore - Laterite Mixture Using Biomass

$$2\text{FeTi}_{2}\text{O}_{5(s)} + \frac{1}{2}\text{O}_{2(g)} \xrightarrow{\text{Below 800°C}} \text{Fe}_{2}\text{TiO}_{5(s)} + 3\text{TiO}_{2(s)}$$
(3)

$$6Fe_{2}TiO_{5(s)} + 6TiO_{2(s)} + \frac{1}{2}CH_{4((g)(CO,H_{2}))} \xrightarrow{below \ 800^{\circ}C} 4Fe_{3}Ti_{3}O_{10(s)} + \frac{1}{2}CO_{2(g)} + 2H_{2}O_{(g)}$$
(4)

In this study, reduction temperatures were increased to the range of 800 - 900 °C in the presence of the syngas. The rutile and metallic iron were formed as shown in equation 5 to 7.

$$\operatorname{Fe}_{2}\operatorname{Ti}_{3}\operatorname{O}_{9(s)} \xrightarrow{800-900^{\circ}\mathrm{C}} \operatorname{Fe}_{2}\operatorname{TiO}_{5(g)} + 2\operatorname{TiO}_{2(s)}$$
(5)

$$\operatorname{FeTiO}_{3(s)} + \operatorname{CO}_{(g)}(\operatorname{H}_{2}, \operatorname{CH}_{4}) \xrightarrow{800 - 900^{\circ}\mathrm{C}} \operatorname{TiO}_{2(s)} + \operatorname{Fe}_{(s)} + 2\operatorname{CO}_{2(g)}(\operatorname{H}_{2}\mathrm{O})$$
(6)

$$Fe_{3}TiO_{6(s)} + 4CO_{(g)} \xrightarrow{800-900^{\circ}C} 3Fe_{(s)} + TiO_{2(s)} + 4CO_{2(g)}$$
(7)

Table 4. Magnetic Separated Sample After Reduction of the Ore - Laterite Mixture Using Biomass

Sample Reference	SiO <sub>2</sub>	$Al_2O_3$	CaO	MgO	Na <sub>2</sub> O	K <sub>2</sub> O	${\rm TiO}_2$	MnO	Fe <sub>2</sub> O <sub>3</sub>	Cu
3230	19.45	3.43	2.98	3.89	1.72	2.34	0.02	0.28	49.3	10.42
3231	11.71	2.93	7.54	3.39	4.71	5.91	0.03	0.05	53.7	4.97
3232	17.66	5.77	3.74	1.94	3.61	4.91	0.01	0.48	52.9	2.1
3233	8.32	4.32	11.94	2.83	5.39	7.03	0.04	0.71	48.3	5.38
3242	17.37	3.42	5.85	1.93	2.43	4.21	0.02	0.85	47.8	6.85
Table								Aixture Us	ing Biomas	s
								Mixture Us MnO	ing Biomas Fe <sub>2</sub> O <sub>3</sub>	s Cu
Table Sample	5. Non-M	lagnetic Se	parated Sar	nple After l	Reduction of	of the Ore -	- Laterite N		0	
Table Sample Reference	5. Non-M SiO <sub>2</sub>	Iagnetic Se Al <sub>2</sub> O <sub>3</sub>	parated Sar CaO	nple After l MgO	Reduction of Na <sub>2</sub> O	of the Ore - K <sub>2</sub> O	- Laterite M TiO <sub>2</sub>	MnO	Fe <sub>2</sub> O <sub>3</sub>	Cu
TableSampleReference3230	5. Non-M SiO <sub>2</sub> 48.09	Iagnetic Se Al <sub>2</sub> O <sub>3</sub> 16.59	parated Sar CaO 13.1	nple After I MgO 4.22	Reduction on Na <sub>2</sub> O 9.21	of the Ore - K <sub>2</sub> O 8.32	Laterite M TiO <sub>2</sub> 2.62	MnO 0.96	Fe <sub>2</sub> O <sub>3</sub> 5.83	Cu 4.8
TableSampleReference32303231	5. Non-M SiO <sub>2</sub> 48.09 56.14	Iagnetic Se Al <sub>2</sub> O <sub>3</sub> 16.59 11.32	parated Sar CaO 13.1 15.49	mple After I MgO 4.22 13.4	Reduction of Na <sub>2</sub> O 9.21 1.18	of the Ore - K <sub>2</sub> O <u>8.32</u> 5.51	- Laterite M TiO <sub>2</sub> 2.62 1.68	MnO 0.96 1.12	Fe <sub>2</sub> O <sub>3</sub> 5.83 10.9	Cu 4.8 3.6

 Table 6.
 Comparison of Percentage Rutile Per Ore After Concentration

Sample Reference	% TiO <sub>2</sub> In Raw sample	% TiO <sub>2</sub> in laterite (0.0054g)	% TiO <sub>2</sub> in ore - laterite mixture before heat treatment	% TiO <sub>2</sub> in ore, laterite & biomass mixture (magnetic)	% TiO <sub>2</sub> in ore, laterite & biomass mixture (tailing)	% TiO <sub>2</sub> increase after ore, laterite & biomass separation
3230	0.41	0.27	0.40	0.02	2.62	2.22
3231	0.46	0.27	0.45	0.03	1.68	1.23
3232	1.13	0.27	1.07	0.01	3.18	2.11
3233	0.91	0.27	0.86	0.04	2.41	1.55
3242	0.28	0.27	0.28	0.02	2.28	2.00

The reduction of the ore-laterite mixture using biomass was done using the optimized parameters and results given in table 4 and 5. Comparison of the percentage results is given in table 6.

The results from table 4 shows that iron concentrate generally increased while rutile decreased significantly in all the ore samples. In table 5 rutile, silica and alumina composition increased significantly in the tailing and reduced in the concentrate making the method of concentration successful. The results from table 6 show that rutile composition increased from about 0.40% in raw (sample 3230) to about 2.62% in the tailing after concentration. This composition represents 2.22% increase after concentration. The increase has been contributed by 0.27±0.01 value of rutile from the laterite. Since the concentration of rutile in the concentrate is very low (0.02-0.04%), then the method is good for the concentration of rutile from ores. The lateritic materials can therefore be used to enrich titanium minerals from ores with low iron content during rutile concentration.

## 4. Conclusions

Laterite soils rich in iron can be used to concentrate rutile from titanium ores with little composition of iron. The method improves rutile concentration with about 1.2 to 2.22%. The method is also suitable as it helps to clean the environment of the biomass waste especially municipal waste.

# **Conflicts of Interest**

The authors declare no conflicts of interest.

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